

***Tower isntalling on Roof buidling
For (25 m) height***

Prepared by :

Eng. Rebwar Ali Hussain

ID in KEU: 4440

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Building Analysis

Based on my practical experiences on the field in the last (6) years of my duties, I would like to state one of the cases that we have executed. This is to be my search report as our calculation & formula is calculated in hereunder report.

Site topology:

- * Roof top site
- * Building (2) story with 3m height for each floor
 - * Skeleton building
 - * Installed (25m) tower (Matis type)
- * Applying reduction factor by (80%) for additional tower loading to minimize its height & antennas mounting



Commerical building checking to support 30 m Steel Tower

The commerical building located at Erbil city-with two stories

1 – Check thickness of the slab:

maximum panel size (5.20 x 7.90 m c/c)

$$t_{\min} = [Ln (0.8 + (fy / 1400))] / [36 + 9 \beta] , \text{ACI } 2008, \text{ Chap.9, Eq. 9.13}$$

$$Ln = 7.9 - 0.8 = 7.0 \text{ m}$$

$$fy = 414 \text{ Mpa (Grade 60),}$$

$$\beta = Ln^1 / Ln^2 = 7.0 / 4.8 = 1.0625$$

$$t_{\min} = [7.0 (0.8 + (414 / 1400))] / [36 + 9 (1.0625)] = 0.164 \text{ m}$$

For this panel thickness to be not less than 14 cm

For the panel which steel tower to be supported on, is 5.2 x 3.3 m c/c as shown in Fig.(1).

$$\beta = 4.8 / 2.9 = 1.655$$

$$t_{\min} = 0.104 \text{ m}$$

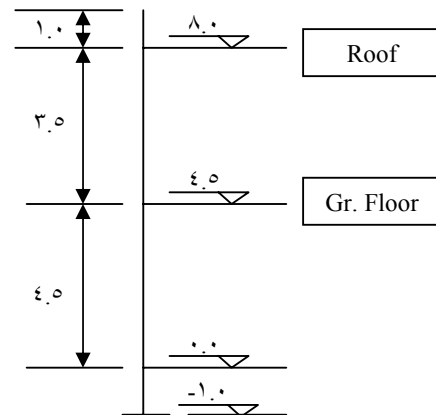
Thickness of 10 cm is adequate for this panel.

۲ - Load Calculations :

The building is consist of two – stories , Ground and Roof , the load can be calculated as follows :

a – Ground Floor :

- Dead Loads.
 - slab, $۰.۱۵ \times ۲۴ = ۳.۶ \text{ kN/ m}^۲$
 - tile + mortar = $۱.۶۲ \text{ kN/ m}^۲$
 - finishing = $۰.۳ \text{ kN/ m}^۲$
-
- $۵.۵۲ \text{ kN/ m}^۲$



$$\text{Live Load} = ۳.۰ \text{ kN/ m}^۲$$

$$\begin{aligned} W_u &= ۱.۲ \text{ D.L} + ۱.۶ \text{ L.L} \\ &= ۱.۲(۵.۵۲) + ۱.۶(۳) = ۱۱.۴ \text{ kN/ m}^۲ \end{aligned}$$

b – Roof

Dead Loads

- slab, $۰.۱۵ \times ۲۴ = ۳.۶۰ \text{ kN/ m}^۲$
- Roofing system (Future) $\approx ۲.۰۰ \text{ kN/ m}^۲$
- finishing $\approx ۰.۳۰ \text{ kN/ m}^۲$

$۵.۹۰ \text{ kN/ m}^۲$

$$\text{Live Load} = ۱.۵ \text{ kN/ m}^۲$$

$$\begin{aligned} W_u &= ۱.۲ \text{ D.L} + ۱.۶ \text{ L.L} \\ &= ۱.۲(۵.۹) + ۱.۶(۱.۵) = ۹.۴۸ \text{ kN/ m}^۲ \end{aligned}$$

-Beam Cross – Sections:

400 x 600 mm Ground

400 x 450 mm Roof

h_{\min} required according to ACI Code chap. 9

For span 7.9 m, $h_{\min} = L / 18.0 = 7.9 / 18.0 = 0.43$ m

For span 0.2 m, $h_{\min} = L / 18.0 = 0.2 / 18.0 = 0.28$ m

Section sizes provided greater than required by ACI Code, there is no need for check of deflection for beams.

Transmission of loads from the slab to B₁ and B₂:

1 – load from the slab

a – roof slab, $W_u = 9.48$ kN / m²

Area bounded by beam B₁ & B₂ shown in Fig.(2)

Area bounded by B₁ = 12.62 m²

Area bounded by B₂ = 0.40 m²

Ultimate load from slab, for B₁ = (12.62 / 0.2) x 9.48 = 23 kN / m

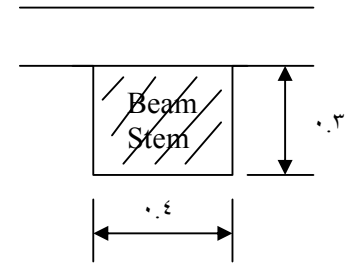
for B₂ = (0.40 / 3.3) x 9.48 = 10.6 kN / m

Beam stem = 0.4 x 0.3 x 24 x 1.2 = 3.0 kN / m



$$B^1, W_u = 23.0 + 3.0 = 26.0 \text{ kN/m}$$

$$B^2, W_u = 10.6 + 3.0 = 13.6 \text{ kN/m}$$



$$b - \text{Ground Floor slab}, W_u = 11.5 \text{ kN/m}^2$$

$$\text{Load from slab to } B^1 = (12.62 / 0.2) \times 11.5 = 27.7 \text{ kN/m}$$

$$B^1, W_u = 27.7 + 3.0 = 30.7 \text{ kN/m}$$

$$\text{Load from slab to } B^2 = (0.40 / 3.3) \times 11.5 = 14.8 \text{ kN/m}$$

$$B^2, W_u = 14.8 + 3.0 = 17.8 \text{ kN/m}$$

Load calculations for Columns:

First the load of beams supported by C^1 & C^2 calculated and shown in Fig.(3), for both ground and roof slab.

$$\text{Load from roof to } C^1 = 30.0 \times 2.6 + 13.6 \times 1.60 + 26.0 \times 4.8 = 238 \text{ kN}$$

$$\text{Load from ground to } C^1 = 36.6 \times 2.6 + 17.8 \times 1.60 + 30.7 \times 4.8 = 282 \text{ kN}$$

$$\text{Col. load} = 0.4 \times 0.4 \times 8 \times 24 \times 1.2 = 37 \text{ kN}$$

$$P_{C1} = 557 \text{ kN}$$

$$\text{Load from roof to } C^2 = 30.0 \times 2.6 + 13.6 \times 1.60 + 26.0 \times 6.00 = 284.4 \text{ kN}$$

$$\text{Load from ground to } C^2 = 36.6 \times 2.6 + 17.8 \times 1.60 + 30.7 \times 6.00 = 336.3 \text{ kN}$$

$$\text{Col. load} = 0.9 \times 0.9 \times 8 \times 28 \times 1.2 = 27 \text{ kN}$$

$$P_{c2} = 60.8 \text{ kN (Ultimate factored load)}$$

Applied moments to the Columns

Columns above ground slab

$$P_{c2} = 288.8 + 18.0 = 306.8 \text{ kN}$$

$$M_x = (1/10) \times 30.0 \times (0.20 - 0.8)^2 - (1/11) \times 19.1 \times 2.9^2 = 0.7 \text{ kN.m}$$

$$M_y = (1/10) \times 26.0 \times 7.0^2 - (1/11) \times 26.0 \times 8.8^2 = 9.8 \text{ kN.m}$$

$$P_{c1} = 238 + 18.0 = 256 \text{ kN}$$

$$M_x = 0.7 \text{ kN.m}$$

$$M_y = (1/10) \times 26.0 \times 8.8^2 - (1/11) \times 26.0 \times 3.6^2 = 3.0 \text{ kN.m}$$

Design of the slab, beam, column and Footings

1 – Check the structural design of the slab.

For the shaded area :



$$W_u = 11.8 \text{ kN/m}^2 \quad f_y = 414 \text{ MPa} \quad f_c' = 21 \text{ MPa}$$

$$t = 100 \text{ mm} \quad \implies d = 100 - 20 - 12/2 = 119 \text{ mm}$$

$$b = 1.0 \text{ m}$$

Calculate m_{neg} and m_{pos} by YLT or other methods:

$$\Sigma W\delta = 11.8 (0.0 \times 3.3 \times 1.70 \times \delta/3 + 0.0 \times 1.70^2 \times \delta/3 \times 2 + \delta/2 \times 1.9 \times 1.70)$$

$$\Sigma W\delta = 39 \text{ kN}$$

$$\Sigma M_{\square} = (m_n + m_p) [3.3 \times \delta/(1.70) + 0.2 \times \delta/(1.70)]$$

$$\Sigma M_{\square} = \Sigma W\delta$$

$$m_n = 0.1 \times 39 \text{ (safety)} = 3.9 \text{ kN.m/m}$$

$$R = M_u / \Phi b d^2 = 0.79 \text{ MPa}$$

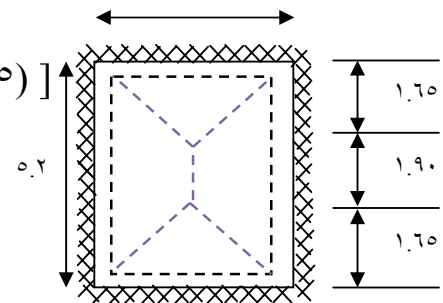
$$m = f_y / 0.80 f_c' = 23.20$$

$$\rho = 1/m (1 - \sqrt{1 - 2mR/f_y}) = 0.00190$$

$$\rho_{\text{calculated}} = 0.00190 > \rho_{\text{min}} = 0.0018 \text{ (ACI Code 7.12)}$$

$$\text{As required} = \rho \times b \times d = 232 \text{ mm}^2/\text{m}$$

$\Phi 10 @ 200 \text{ mm c/c}$ required.



Comment: Provided reinforcement more than required i.e the slab is safe and there is no additional loads from steel tower to the slab.

2 – Check the structural design of beams:

more critical beam is B1, L = 0.2 m c/c

$$M_{neg.} = 1/11 W_u l_n^2 = 1/11 \times 26.5 \times (0.2 - 0.8)^2 = 0.5 \text{ kN.m}$$

(ACI Code 2008 chap. 8)

$$b = 400 \text{ mm}$$

$$d = 400 - 40 - 10 - 16/2 = 392 \text{ mm}$$

$$R = M_u / \Phi b d^2 = 1.0 \text{ MPa}$$

$$\rho = 1/m (1 - \sqrt{1 - 2mR/f_y}) = 0.020 < \rho_{min}$$

Use ρ_{min}

$$\rho_{min} = 0.20 \sqrt{f_c'} / f_y = 0.028 < 1.4 / f_y = 0.0338$$

$$\rho_{min} = 0.0338$$

$$A_s = \rho b d = 0.0338 \times 400 \times 392 = 530 \text{ mm}^2$$

Provide reinf. 4Φ 16 mm, $A_s = 804 \text{ mm}^2 > 530 \text{ mm}^2$ O.K

Comment: 1 – Beam B1 resisting applied load safely.

2 – When additional loads applied from the steel tower, the additional loads to be resisted by Other Beam shown in Fig.(4) from analysis by STAAD Pro 2007 Software to transmit the loads to the Columns.

3 – Check structural design of the Columns :

Applied load from slab and Beam to Pc2 (more critical column)

a – C2 (Roof Column)

$$P_{c2} = 2.2 \text{ kN}$$

$$\left. \begin{array}{l} M_x = 0.7 \text{ kN.m} \\ M_y = 9.4 \text{ kN.m} \end{array} \right\} \text{ greater than } M_{\min}, \text{ i.e to be considered}$$

Design the Column as biaxial column

$$e_x = M_y / P = 31.0 \text{ mm}, e_x / h = 0.110$$

$$e_y = M_x / P = 1.11 \text{ mm}, e_y / h = 0.003$$

$$\text{Columns } 400 \times 400 \text{ mm}, A_s = \rho_g \times 400 \times 400 = 160.8 \text{ mm}^2$$

$$\rho_g = 160.8 / (400 \times 400) = 0.1\%$$

$$\gamma = (400 - 75 \times 2) / 400 = 0.7$$

From charts given in the text book by Arthur H. Nilson "Design of concrete structures" 2004.

$$P_u = 0.14 f_c' A_g = 470.4 \text{ kN} > 3.3 \text{ kN O.K}$$

$$M_x = 0.13 f_c' A_g h = 176.0 \text{ kN} > 9.4 \text{ kN O.K}$$

$$M_y = 0.10 f_c' A_g h = 20.0 \text{ kN} > 0.7 \text{ kN O.K}$$

Comment: 1- Columns are adequate for holding the building safely

2- Additional load comes from the Tower is less than

$$(470.4 - 3.3) = 467.1 \text{ kN}, \text{ O.K safe}$$

No Additional treatment reqd. (Detail calculation given in the output of the Program.)

ε – Check for Footing :

$$\text{maximum applied load from } C_2 \text{ to foundation is } P_{c2} = 608 \text{ kN}$$

Note: Based on soil investigation for other building in Gulan & Ainkawa

$$\text{Site, Allowable bearing capacity, } q_{\text{all}} \approx 100 - 200 \text{ kN/m}^2$$

$$\text{For calculations, } q_{\text{all}} \approx 170 \text{ kN/m}^2$$



Unfactored load, $P_{cr} = 108 / 1.2 = 90 \text{ kN}$

Area reqd. = $90 / 170 = 0.53 \text{ m}^2$

Area Provided $1.8 \times 1.8 = 3.24 > 0.53 \text{ O.K}$

Check punching shear strength and calculate thickness of footing:

Required thickness based on the applied load:

$$108 = (0.75 / 3) \sqrt{f_c'} \times d \times (1.2 + d) \times 1$$

$$d = 22 \text{ cm}$$

$t = 22 \text{ cm}$ on Lean Concrete

thickness provided $> t$ reqd. O.K

$$A_s = 1.8 \times 1.8 \times 1.2 = 3.89 \text{ mm}^2 \text{ (} \Phi 16 @ 20 \text{ mm c/c)}$$

To prevent punching shear failure, 22 cm thickness required.

Comment :

1- **Footing dimensions & reinf. is adequate for the existing Building.**

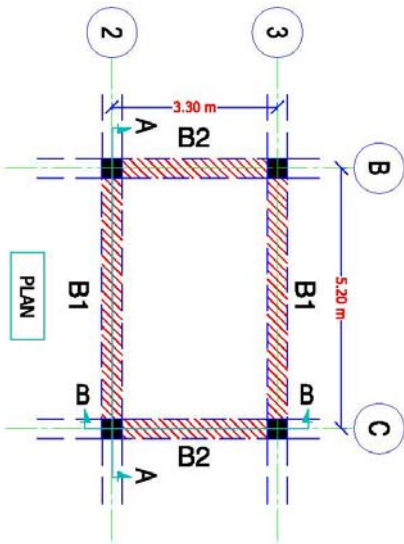
Check structural design when steel tower loads applied.



- ١- slab , no need for check, since the loads goes directly to beams & columns.
- ٢- Beams, provided beams not adequate to resist additional loads, other sections added as shown in the detail drawings and mentioned earlier.
- ٣- Columns with $\xi \cdot \cdot \cdot \times \xi \cdot \cdot \cdot$ and $\wedge \Phi \ ١٦$ mm reinforcement.
- ٤- Provided Area of Footing **more** than reqd. after additional loads applied.

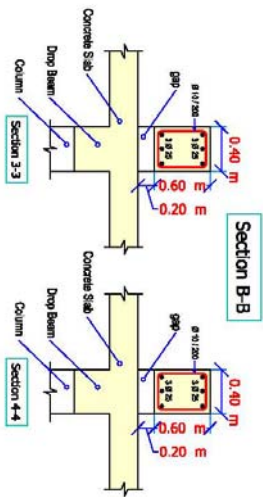
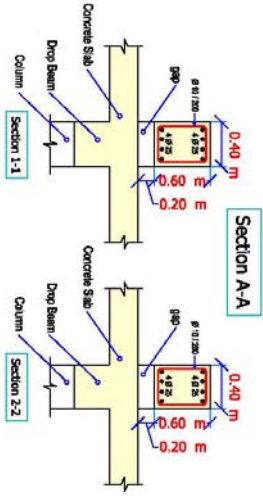
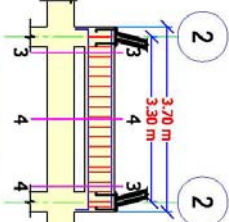
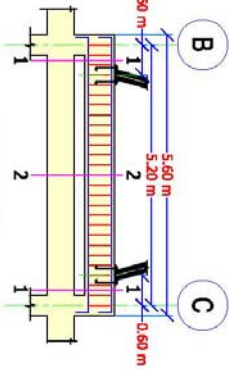
Note: Aditonal loads from steel tower provided by Asia Cell with reduction factor of % $\wedge \cdot$ (According to Instructions of Mr. Rebware).

Thanks



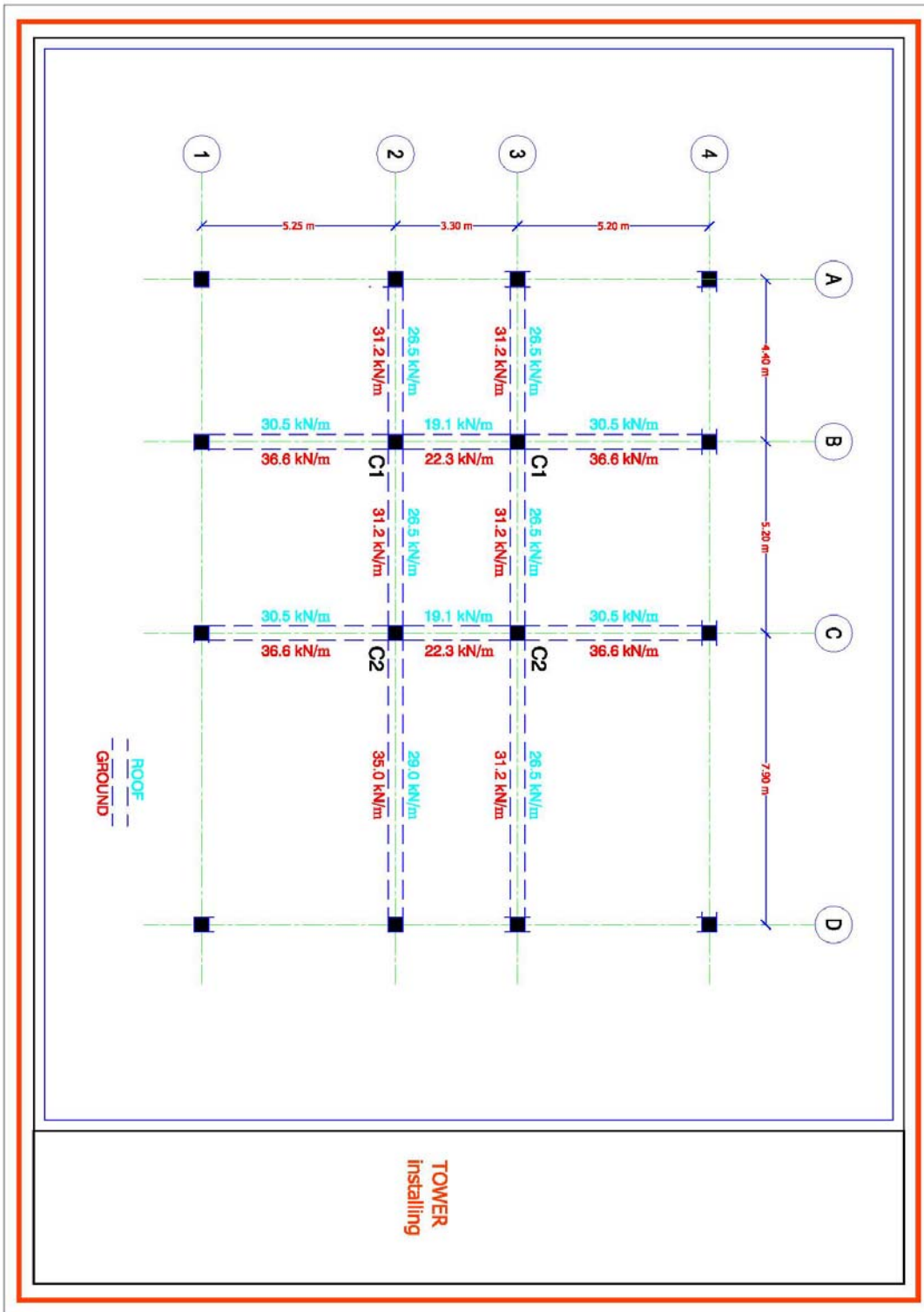
Note :
Amount of Steel required :

- 1- \varnothing 25 mm \rightarrow 16 No. of 6.0 m Length
- 2- \varnothing 25 mm \rightarrow 12 No. of 4.0 m Length
- 3- \varnothing 10 mm for stirrups 90 Stirrups



TOWER
installing





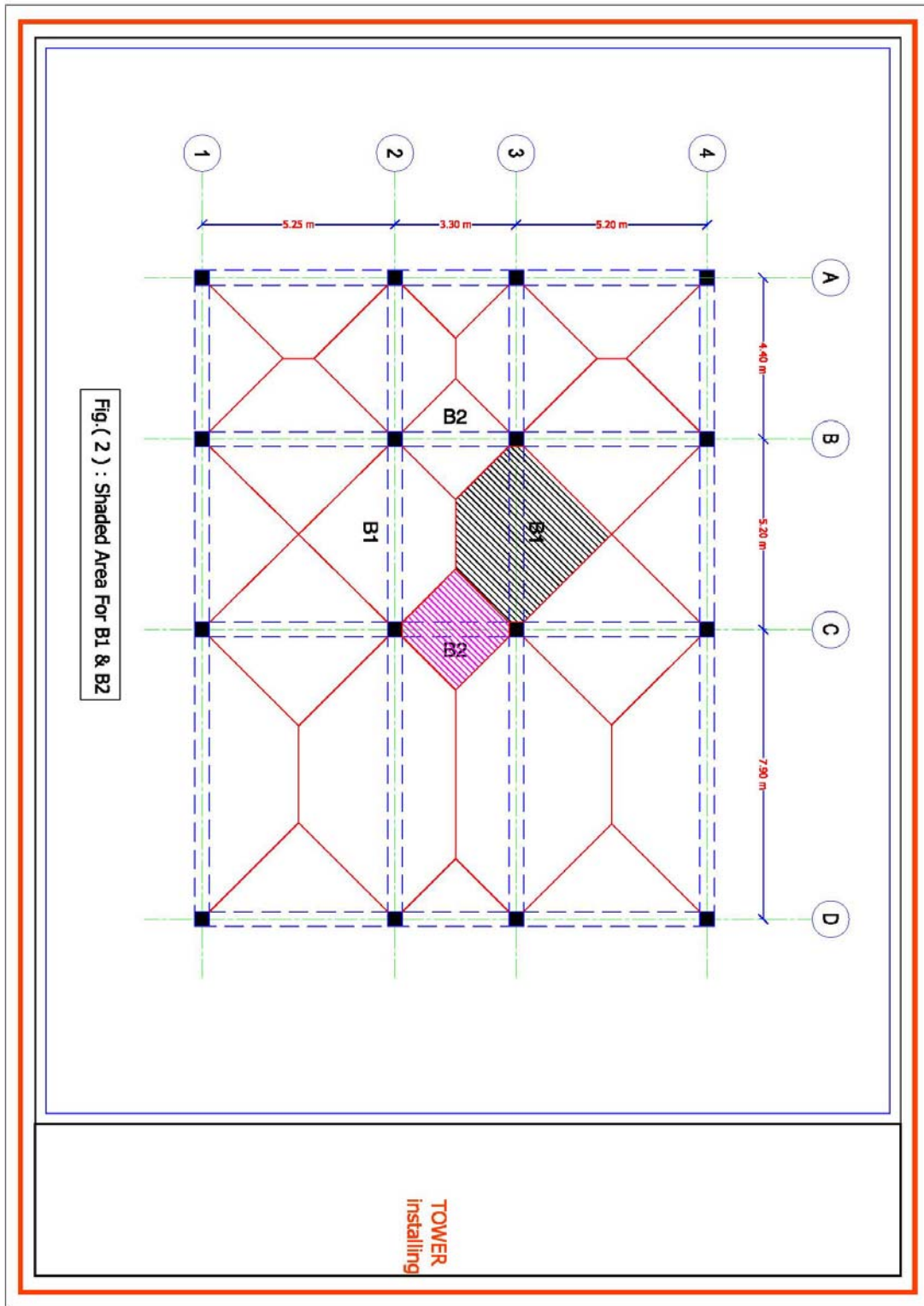


Fig. (2) : Shaded Area For B1 & B2

TOWER
Installing

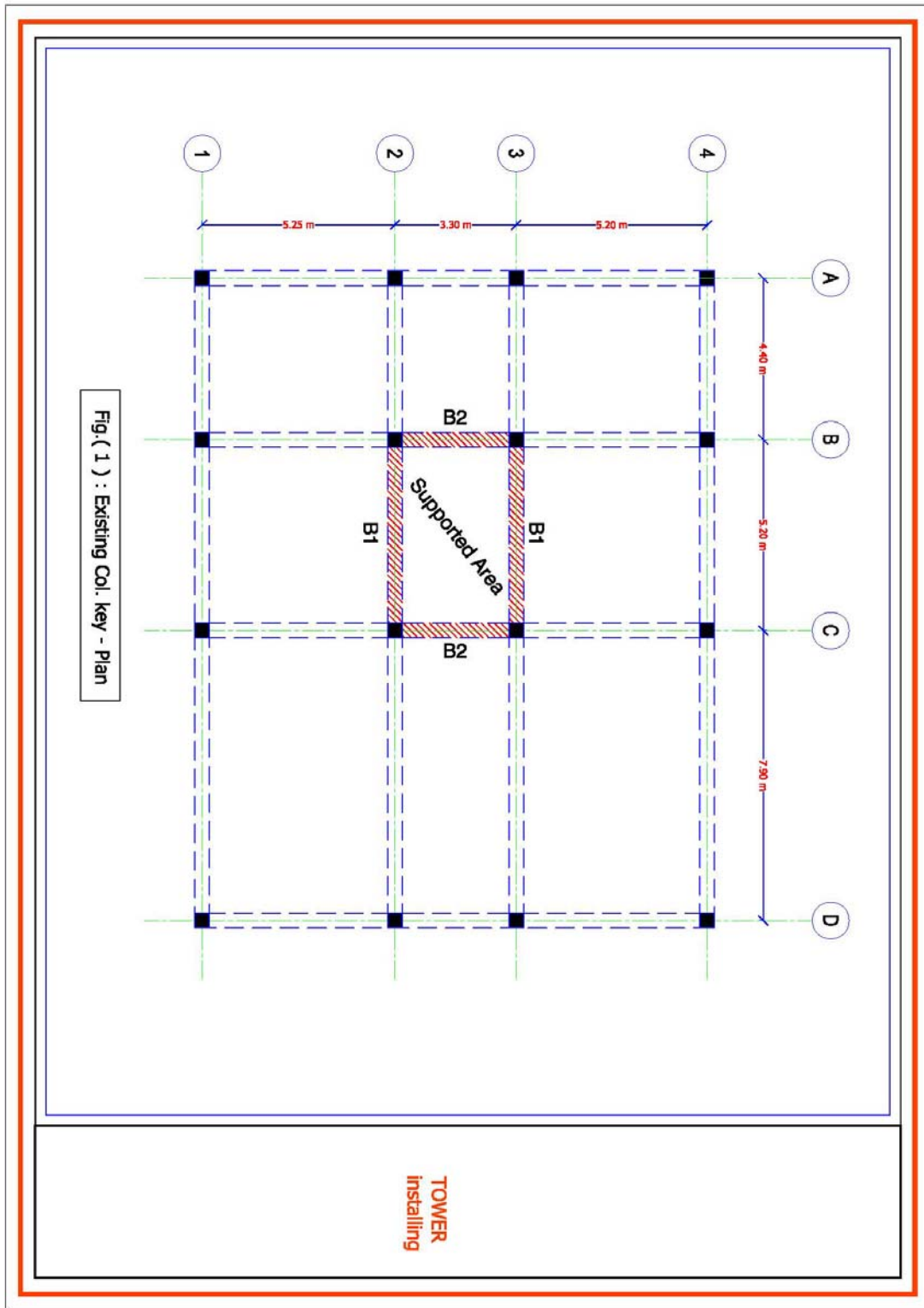


Fig.(1) : Existing Col. key - Plan